# **MEMORANDUM**

# State of Alaska

# Department of Transportation & Public Facilities Northern Region Preconstruction

**TO:** Chris Johnston, P.E.

Engineering Manager

Northern Region

THRU: Kevin Maxwell 310 F. KF~

Regional Engineering Geologist

Northern Region

FROM Tim Weiss TW

Engineering Geologist

Northern Region

DATE: September 4, 2013

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\report\obstruction area memo.doc

**TELEPHONE** 458-6883

NO:

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SUBJECT: Ambler Airport

Rehabilitation

**Geotechnical Investigation** 

Addendum AKSAS 60262

## **SUMMARY**

This memorandum is based on the Northern Regions Material Section (NRMS) Geotechnical Report, "Ambler Airport Rehabilitation and Ambler Sewage Lagoon Road" Report dated June 2013, and at your request. This memo is an addendum to the above referenced report and provides additional geotechnical information pertaining to the planned terrain obstruction removal area of the Ambler Airport project.

As part of the Airport Rehabilitation project, the terrain obstruction area at the southwest corner of the main and crosswind runways is planned to be lowered in elevation to provide aircraft visibility between the two runways (Figure 1). The obstruction area is approximately 10 feet higher in elevation than the runways. It is planned to use the material from the lowering of the obstruction area as borrow material and placed at the main runway expansion area.

We estimate approximately 20 percent of the terrain obstruction area material could have high organic contents and/or natural moisture, additionally we estimate a soil shrinkage factor of approximately 10 to 25 percent after compaction and before excavation for the area.

### GEOTECHNICAL INVESTIGATION AND SUBSURFACE FINDINGS

The terrain obstruction area has an undulating surface with spruce trees up to 6 inches in diameter and overall gradually slopes to the south and southwest. The geotechnical investigation was performed in February 2013, with seven test holes drilled in the area. The obstruction area was snow covered at the time of our investigation with up to 3 feet of snow and some drifting. A small trail was plowed to provide drill rig access. Two of the

AKSAS: 61303 Terrain Obstruction Area Memo

seven test hole locations (TH13-049 and 13-011) were drilled slightly outside the approximate boundary. TH13-011 was mainly drilled to provide subsurface information at the toe of the crosswind runway, this test hole is not included. TH13-048 is located in a disturbed area and lower in elevation than areas to the north, this area could have disturbance related to a nearby weather station and antennas.

All test holes were drilled using a solid stem auger method, with 4.5-inch O.D. augers and samples collected from auger cuttings. These six test holes encountered the following subsurface conditions:

- 1 foot thick organic mat.
- Frozen material was encountered from the surface to 12 feet in depth. TH3-048 was frozen to the depth explored at 15 feet.
- Moisture contents in the frozen material ranged from 7.5 to 16.7 percent. Higher moisture contents were encountered in TH13-048 with 28.4 and 31.8 percent collected in silt material, and a highly organic layer from 2 to 5 feet in depth yielded a moisture content of 115.5 percent.
- Thawed material was encountered in all test holes except TH13-048, and from a consistent depth from 12 to 12.5 and continued to depths explored at 15 feet. Thawed material consisted of silt and fine silty sand.
- Organic contents in frozen material were slight and ranged from 0.2 to 1.1 percent. At TH13-048 the highly organic material encountered from 2 to 5 feet indicated 44.0 percent organics.
- Asbestos sample results ranged from less than 0.1 percent by weight and 12 asbestos structures to less than 0.1 percent by weight and zero asbestos structures.

Visible Ice was not encountered in any test holes in the terrain obstruction area to the depths explored. Frozen material encountered was classified as nonvisible bonded with no excess ice (Nbn), nonvisible bonded with excess ice (Nbe), and poorly bonded or friable (Nf).

### EXPECTED PHYSICAL SITE CONDITIONS

- Expect frozen ground, either seasonally or perennially frozen within the terrain obstruction area at any time of the year.
- Expect perched groundwater on top of frozen layers.
- Expect pumping of silt soils at the bottom of excavations
- Expect ice-rich soils to be present in low areas.
- Expect organic soils in low areas.
- Expect difficulty handling moist or wet thawed silty soils.

# COMMENTS AND RECOMMENDATIONS

Our investigation took place during the winter and surface conditions were not observed in the terrain obstruction area.

- Two different materials were encountered during drilling:
  - 1. A material with low drill resistance that was marginally frozen, poorly bonded and friable. The material was sandy in nature and probably

Ambler Airport Rehabilitation AKSAS: 61303 Terrain Obstruction Area Memo

related to mapped surface dune deposits. This was generally associated with lower natural moistures and higher elevations.

- 2. A material with higher drilling resistance that was frozen and well bonded (TH13-048 only). This material was silty in nature, high moistures, high organics, and generally associated with lower elevations.
- The limits of the two materials are not clearly defined, but in general, the silty material with organics and higher moistures are related to lower areas of the terrain obstruction area.
- Most of the terrain obstruction area drilling encountered marginally frozen, poorly bonded and friable silty sand or sandy silty material.
- This material fails to meet standard specifications for Select Material Type A and B and is frost susceptible with 50.2 to 85 percent passing the #200 sieve. This material can be used where frost susceptible borrow material is acceptable. We estimate approximately 20 percent of the terrain obstruction area material could have excessive organic contents and/or natural moisture.
- Naturally Occurring Asbestos (NOA) testing in the area indicated values below 0.25 percent. Additional Asbestos testing results can be found in the referenced geotechnical report.
- One Proctor value indicated optimum moisture content of 14.6 percent and 103.0 pounds per cubic foot maximum dry density. Samples collected in the area indicated most natural moisture contents in the area are at or near optimum moisture.
- Some material may be above optimum moisture, requiring draining and drying to achieve optimum compaction.
- Optimum compaction is necessary to avoid differential settlement beneath the runway extension areas.
- Based on the results of laboratory testing, the natural state of the subsurface soils in the terrain obstruction area, and the attached letter from 1988, we estimate a soil shrinkage factor of approximately 10 to 25 percent after compaction and before excavation.

Attached are a complete set of test hole logs, laboratory test results for the terrain obstruction area, and a DOT&PF letter dated 1988 and pertaining to the original construction of Ambler Airport.

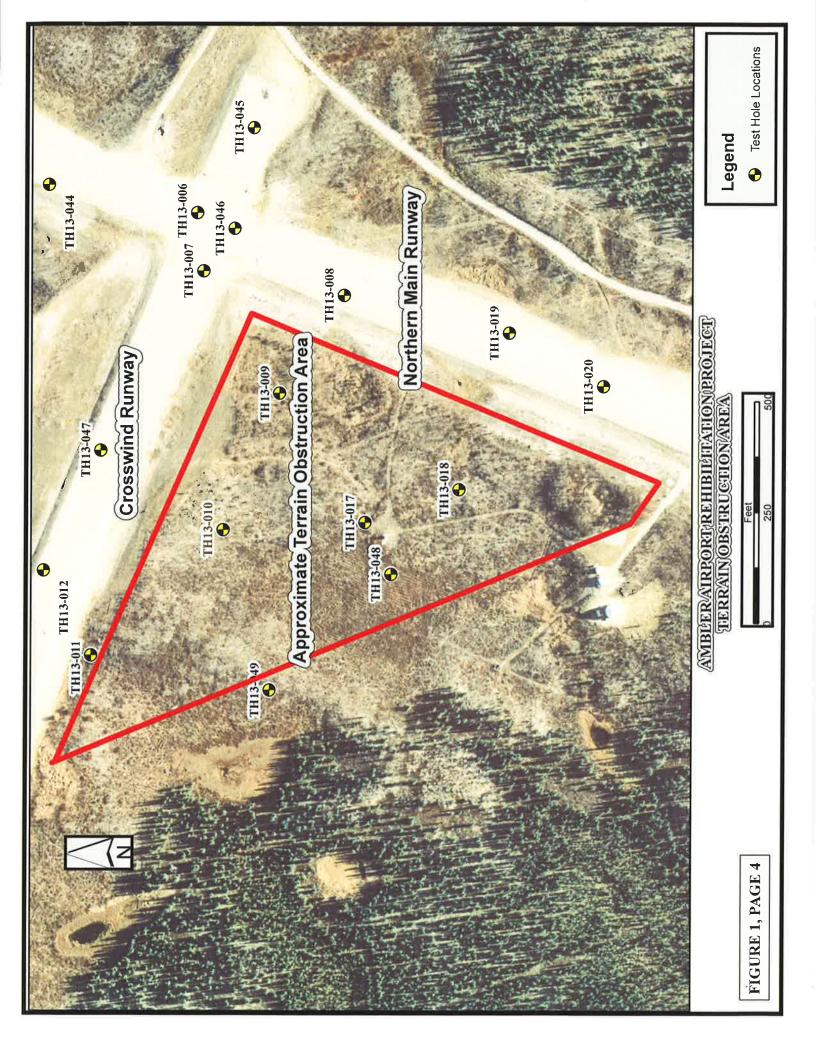
Jeff Currey, P.E.

Materials Engineer

Date

cc: Scott Maybrier, Airport Design

Attachments: Figure 1, test hole logs, lab results, 1988 Ambler letter.



#### **FINAL TEST HOLE LOG** STATE OF ALASKA DOT/PF Northern Region Materials Geology Section Project Test Hole Number TH13-009 Ambler Airport Rehibilation Project Number AKSAS 61303 Total Depth 15 feet Field Geologist T. WEISS **Dates Drilled** 3/1/2013 Field Crew S, Parker and P, Lanihan Equipment Type Mobile B-24 Station, Offset Weather Latitude, Longitude N67\_1066°, W157.8558° cloudy and cold TH Finalized By T. Weiss Vegetation Tundra Elevation Sample Data Ground Water Data GENERAL COMMENTS: While Drilling After Drilling Obstruction area. Located on orginal ground, Depth in (fl.) Drilling Method Depth in (Feet) Sample Inter Log Time Count Date Casing Blows / Method Symbol SUBSURFACE MATERIAL 0 Bn ORG MAT hi Org 1 Tn Silty SAND Nbn 13-221A AUGER 2 SAMPLE 13-2214 (1.8-2.2): 2 3 3 Nf 4 13.2215 5 SAMPLE 13-2215 (4.8-5.2): NM 11.7%, ORG 1.0% 5 Nbn, Interlayered Silt 6 S-S Auger 7 Nf 13.226 AUGER SAMPLE 13-2216 (7.8-8.2): 8 8 31.8 degrees F 9/4/13 9 Tn SILT AKDOT TEST HOLE LOG - USCS LOGS LATEST GPJ NR AKDOT PRECON USCS 06 28 07 GDT 10 SAMPLE 13-2217 (9.0-15.0): ML, 85% -200, NV, NP 10 11 11 13.2217 AUGER AUGER 12 12 moist, loose, 33.5 degrees F 13.2218 13 SAMPLE 13-2218 (12.8-13.2): NM 8.9% 13 14 14 15

CME Auto Hammer

Cathead Rope Method

#### FINAL TEST HOLE LOG STATE OF ALASKA DOT/PF Northern Region Materials Geology Section Project Test Hole Number TH13-010 Ambler Airport Rehibilation Project Number AKSAS 61303 Total Depth 15 feet Field Geologist T. WEISS Dates Drilled 3/1/2013 Field Crew S. Parker and P. Lanihan Equipment Type Mobile B-24 Station, Offset Weather cloudy and cold Latitude, Longitude N67.10695°, W157.85796 TH Finalized By T. Weiss Vegetation Tundra Elevation Sample Data Ground Water Data GENERAL COMMENTS: White Drilling After Drilling Obstruction area. Located on orginal ground, Depth in (ft.) **Drilling Method** Depth in (Feet) Log Time Coun Graphic L Date Method Blow Symbol SUBSURFACE MATERIAL 0 Bn ORG MAT hi Org 13.2219 AUGER SAMPLE 13-2219 (0.8-1.2): Tn Sandy SILT sl Org, Nbn 2 2 SAMPLE 13-2221 (1.5-10.0): ML, 50.2% -200, NV, NP, Max. Density 103 pcf, Opt. Moisture 14.6% 3 3 3-2220 Interlayered silt 4 SAMPLE 13-2220 (3.8-4.2): 5 5 13-2221 AUGER 6 Nf 13-2222 AUGER S-S Auger SAMPLE 13-2222 (6.8-7.2): NM 7.5% 8 8 31.7 degrees F 9/4/13 9 9 AKDOT TEST HOLE LOG - USCS LOGS LATEST GPJ NR\_AKDOT\_PRECON\_USCS\_06\_28\_07.GDT 10 Tn Silty SAND N SAMPLE 13-2223 (10.0-15.0): 11 11 33.2 degrees F 12 12 AUGER SAMPLE 13-2224 (12.3-12.7): 13 13 dry, 33.6 degrees F 14 14 15

CME Auto Hammer

Cathead Rope Method

### **FINAL TEST HOLE LOG** STATE OF ALASKA DOT/PF Northern Region Materials Geology Section Project Ambler Airport Rehibilation Test Hole Number TH13-017 Project Number AKSAS 61303 Total Depth 15 feet Field Geologist \_ T. WEISS Dates Drilled 3/1/2013 Field Crew S. Parker and P. Lanihan Equipment Type Mobile B-24 Station, Offset cloudy and cold Latitude, Longitude N67.10607°, W157.85785 TH Finalized By T. Weiss Vegetation Tundra Elevation Sample Data Ground Water Data GENERAL COMMENTS: Obstruction area. On orginal ground. Depth in (ft.) Depth in (Feet) Time Date Symbol SUBSURFACE MATERIAL 0 Bn ORG MAT hi Org Bn Silty SAND sl Org, Nbn 2 2 3-2231 AUGER SAMPLE 13-2237 (2.3-2,7): 3 3 Nf, 30.2 degrees F 4 13.2238 5 SAMPLE 13-2238 (4.8-5.2): NM 10.9%, ORG 0.2% 6 6 S-S Auger 13.2239 8 SAMPLE 13-2239 (7.8-8.2): 8 AKDOT TEST HOLE LOG - USCS LOGS LATEST GPJ NR\_AKDOT\_PRECON\_USCS\_06\_28\_07.GDT 9/4/13 9 9 31.7 degrees F 10 10 11 11 12 12 dry to moist, 33.1 degrees F (3.2240) 13 SAMPLE 13-2240 (12.8-13,2): NM 14.9% 13 14 14 15 132107 SAMPLE 13-2107 (16.8-17.2):

CME Auto Hammer

Cathead Rope Method

#### FINAL TEST HOLE LOG STATE OF ALASKA DOT/PF Northern Region Materials Geology Section Project Test Hole Number TH13-018 Ambler Airport Rehibilation Project Number AKSAS 61303 Total Depth 15 feet Field Geologist T\_WEISS Dates Drilled 3/1/2013 Field Crew S. Parker and P. Lanihan Equipment Type Mobile B-24 Station, Offset Weather Latitude, Longitude N67.10549°, W157.85733 cloudy and cold TH Finalized By T. Weiss Vegetation Elevation Tundra Ground Water Data Sample Data GENERAL COMMENTS: White Dritting Obstruction area. On orginal ground, Depth in (ft.) **Drilling Method** Depth in (Feet) Time Date Method Graphic Symbol SUBSURFACE MATERIAL 0 Bn ORG MAT hi Org Bn Sandy SILT 13-2241 AUGER sl Org, Nf 2 2 SAMPLE 13-2242 (1.0-7.0): ML, 62.9% -200, ORG 1.1%, NV, NP SAMPLE 13-2241 (1.8-2.2): 3 Tn 3 3.2242 AUGER 4 4 5 5 6 S-S Auger 7 30.8 degrees F 8 3-2243 AUGER 8 SAMPLE 13-2243 (8.2-8.7): 9 Tn Silty SAND 10 10 11 11 LOGS LATEST GPJ NR\_AKDOT\_PRECON\_USCS\_06\_28\_07.GDT\_9/4/13 12 12 moist, 33.6 degrees F 13 13 13-2244 14 SAMPLE 13-2244 (13.8-14.2): 14 15 AKDOT TEST HOLE LOG - USCS

CME Auto Hammer

Cathead Rope Method

#### FINAL TEST HOLE LOG STATE OF ALASKA DOT/PF Northern Region Materials Geology Section Project Ambler Airport Rehibilation Test Hole Number TH13-048 Project Number AKSAS 61303 Total Depth 15 feet Field Geologist \_ T. WEISS **Dates Drilled** 3/1/2013 Field Crew S. Parker and P. Lanihan Equipment Type Mobile B-24 Station, Offset Weather cloudy and cold Latitude, Longitude N67.10591°, W157.85867 TH Finalized By T. Weiss Vegetation Tundra Elevation Ground Water Data Sample Data GENERAL COMMENTS While Drilling After Drilling Obstruction area Depth in (ft.) **Drilling Method** Depth in (Feet) Time Casing Blows / Method Sample N-Value Date Symbol SUBSURFACE MATERIAL 0 Bn ORG MAT hi Org 1 Bn SILT w/ Sand hi Org, Nbn 2 **Bn PEAT** 13.2234 hi Org 3 SAMPLE 13-2234 (2.8-3.2): NM 115.5%, ORG 44.0% 3 4 4 5 Gy SILT w/ Sand Nbe 6 6 (32235 7 SAMPLE 13-2235 (6.8-7.2) NM 31.8%, NV, NP 7 8 8 AKDOT TEST HOLE LOG - USCS LOGS LATEST GPJ NR AKDOT PRECON USCS 06 28 07 GDT 9/4/13 9 9 10 10 11 11 12 12 (3-2236) 13 SAMPLE 13-2236 (12.8-13.2): NM 28.4% 13 14 14 15

CME Auto Hammer

Cathead Rope Method

# **FINAL TEST HOLE LOG**

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# STATE OF ALASKA DEPARTMENT OF TRANSPORTATION **NORTHERN REGION**

LABORATORY TESTING REPORT

PROJECT NAME:

PROJECT NUMBER: AKSAS NUMBER:

Ambler Airport Rehibilation

SAMPLED BY:

61303 T. Weiss

MATERIAL SOURCE:

Terrain Obstruction Area

TEST HOLE NUMBER DEPTH (feet) LATITUDE LONGITUDE LAB NUMBER DATE SAMPLED	TH13-009 4.8-5.2 N67.1066° W157.8558° <b>13-2215</b> 1-Mar-13	TH13-009 9.0-15.0 N67.1066° W157.8558° <b>13-2217</b> 1-Mar-13	TH13-009 12.8-13.2 N67.1066° W157.8558° <b>13-2218</b> 1-Mar-13	TH13-010 1.5-10.0 N67.10695° W157.85796° 13-2221 1-Mar-13	TH13-010 6.8-7.2 N67.10695° W157.85796° 13-2222 1-Mar-13	TH13-017 4.8-5.2 N67.10607° W157.85785° <b>13-2238</b> 1-Mar-13	TH13-017 12.8-13.2 N67.10607° W157.85785 <b>13-2240</b> 1-Mar-13
% Passing 3" 2" 1.5" 1.0" 0.75" 0.5" 0.375" #4		-					
#8 #10 #16 #30 Sand #40 #50 #60 #80		100 99 99 98		100 99 99 98 97			
Silt/Clay #200		85.0		50.2			
Hydro 0.02 0.005 0.002 0.001						G.	
LIQUID LIMIT PLASTIC INDEX USCS CLASSIFICATION		NV NP ML		NV NP ML			
USCS SOIL DESCRIPTION	(SiSa)	Si	(SiSa)	SaSi	SaSi	(SiSa)	(SiSa)
NATURAL MOISTURE ORGANICS SP. GR. (FINE) SP. GR. (COARSE) MAX. DRY DENSITY OPTIMUM MOISTURE L.A. ABRASION DEGRAD. FACTOR SODIUM SULF. (CRSE) NORDIC ABRASION	11.7 1.0		8.9	2.66 103.0 14.6	7.5	10.9 0.2	14.9
REMARKS				T-99 was			

GENERAL COMMENTS

Gradation is based on material passing the 3" sieve, according to Alaska Test Method T-7.

(30il descriptions shown in parentheses are based on field determinations.)

 $USCS \ Soil \ Description \ Abbreviations: \ WG = Well-graded; \ PG = Poorly-graded; \ E = Elastic; \ L = Lean; \ F = Fat$ 

<sup>&</sup>lt;sup>1</sup> Organic content determination is based on the results of the ATM T-6 test method.

### STATE OF ALASKA DEPARTMENT OF TRANSPORTATION NORTHERN REGION LABORATORY TESTING REPORT

PROJECT NAME:

Ambler Airport Rehibilation

PROJECT NUMBER:

61303 T. Weiss

AKSAS NUMBER: SAMPLED BY:

Tor

MATERIAL SOURCE:

Terrain Obstruction Area

TEST HOLE DEPTH (feet) LATITUDE LONGITUDE LAB NUMBE DATE SAMP	) <i>R</i>	TH13-049 2.0-10.0 N67.10666° W157.8605° <b>13-2232</b> 1-Mar-13	TH13-049 14.2-14.8 N67.10666° W157.8605° 13-2233 1-Mar-13	TH13-048 2.8-3.2 N67.10591° W157.85867° 13-2234 1-Mar-13	TH13-048 6.8-7.2 N67.10591° W157.85867° <b>13-2235</b> 1-Mar-13	TH13-048 12.8-13.2 N67.10591° W157.85867° 13-2236 1-Mar-13	TH13-018 1.0-7.0 N67.10549° W157.85733° <b>13-2242</b> 1-Mar-13	
% Passing Gravel	3" 2" 1.5" 1.0" 0.75" 0.5" 0.375"							
Sand	#8 #10 #16 #30 #40 #50 #60 #80 #100	100 98 96 89 83					100 99 99 97 96	
Silt/Clay	#200	51.4					62.9	
Hydro	0.02 0.005 0.002 0.001							
LIQUID LIMIT PLASTIC IND USCS CLASS	EX	NV NP ML			NV NP		NV NP ML	
USCS SOIL D	DESCRIPTION	SaSi	(SiSa)	(Pt)	(Si w/Sa)	(Si w/Sa)	SaSi	
NATURAL MO ORGANICS SP. GR. (FINI SP. GR. (COA MAX. DRY DE OPTIMUM MO L.A. ABRASIO DEGRAD. FA SODIUM SUL NORDIC ABR	E) ARSE) ENSITY DISTURE DN CTOR .F. (CRSE) .F. (FINE)	0.8	9.4	115.5 44.0	31.8	28.4	1.1	
REMARKS				hi Org <sup>1</sup>				
			<u> </u>					

GENERAL COMMENTS

Gradation is based on material passing the 3" sieve, according to Alaska Test Method T-7,

(Soil descriptions shown in parentheses are based on field determinations.)

 $USCS \ Soil \ Description \ Abbreviations: \ WG = Well-graded; \ PG = Poorly-graded; \ E = Elastic; \ L = Lean; \ F = Fat$ 

Organic content determination is based on the results of the ATM T-6 test method.

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tate of Alaska

Department of Transportation & Public Facilities

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TO: Rod Platzke

Design Group Chief Northern Region

DATE: November 28, 1988

FILE NO: 244N:

TELEPHONE NO: 451-2230

FROM:

Hal Livingston Sr. Engineering Geologist Northern Region

Subject: Shrinkage in silt soils used in embankments

The wind-blown silt at Ambler was used in constructing the runway embankment in 1977. Several in-place densities of the silt borrow (primarily in the ditch areas) were taken during construction and compared with the densities of the compacted embankment. As would be expected, the first lifts of silt placed on uncompacted soil did not achieve 95 percent compaction. Later lifts gradually achieved higher rates of compaction until a 96 percent compaction was reached. Comparison of the in-place density with that achieved in construction shows that the in-place volume of the wind-blown silt ranged from 9.2 to 15.4 percent higher than when compacted into the runway embankment. The average indicated shrink was 11.7 percent for the wind-blown silt at Ambler. These figures are based on the construction data attached.

Additional tests with the Nuclear densometer and the Washington densometer were taken at Ambler on October 13, 1988. These tests were run in three locations along the proposed cross-wind runway where cuts will be made to supply material for the embankment. Knowledge of the expected decrease in volume from in-place yards to embankment yards will help the designers set grades and backslopes. Contractors will also know more closely how many yards they will have to excavate in order to construct the embankment.

The shrinkage percentage between tests ranged from 11.5 to 23.0 and averaged 15.6 percent. If 200,000 cubic yards of material is to be placed in the embankment, then approximately 237,000 cubic yards will have to be excavated to supply this quantity. It is probable that there is natural variation in the in-place density of wind-blown silt at Ambler and the actual number of yards required for the embankment may be above or below that estimated based on these tests. This small number of tests cannot quarantee precise quantities, because there is some variation in the shrinkage factors between test locations, but the tests should aid considerably in reducing the unknown factors.

At Chalkyitsik much less data is available but it indicates that shrink of the in-place alluvial silt and silty sand is 34.5 percent when compacted into the runway embankment. This large shrinkage may result from several processes acting on the soil but the chief cause is probably fluffing of

the material by the action of seasonal freezing; in other words, the formation of taber ice in successive cycles over a very long time (thousands of years). The presence of volcanic ash in the surface layer of wind-blown silt probably has helped this fluffing process.

The conditions for taber ice formation are ideal in that the materials are composed of silt containing a high percentage of .02 and .005 sizes (from the volcanic ash). The presence of permafrost 7 to 8 feet below the surface results in retention of moisture within the zone of seasonal freezing and provides a resevoir of water needed to form abundant taber ice lenses.

Successive freeze-thaw cycles would move larger particles to the surface and position them in sorted stone rings or even sand rings. Several examples of both features were observed in the exposures in the side borrow areas at the Chalkyitsik Airport.

There is evidence in the area (burned trees and stumps) that recent forest fires could have resulted in the removal of shading trees and complete destruction of the insulating moss layer. Subsequent melting of perennially frozen soils only a few years ago could have left the soils less compacted than they would be after several tens of years.

# CONCLUSION

The very loose soils at Chalkyitsik are probably the result of fluffing of the soil resulting from successive freeze and thaw and the accumulation of taber ice within the fine-grained soils. Forest fires, that later removed the insulating trees and moss, resulted in melting of the ice. Drainage of much of the moisture from the thawed soils left them with a very low density.

Geologists with the Department need to be aware of these potential problems in fine-grained soils so that adequate sampling can be done to alert Designers, Bidders, and construction personnel to the presence of material with unusually high shrinkage.

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Attachments: Lab tests.

xc: Paul W. Misterek, Materials Engr Monte K. Weaver, Chief, Geotech. Services Jim Elieff, Design John Miller, Design Dave McCaleb, Construction Chief Orlen Entzel, Construction Group Chief Mike Grahek, Materials Gary Brazo, Materials Peter Ondra, Materials Tim Woster, Materials